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# Investigation of $(CeO_2)_x(Sc_2O_3)_{(0.11-x)}(ZrO_2)_{0.89}$ (x = 0.01-0.10) electrolyte materials for intermediate-temperature solid oxide fuel cell

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# ABSTRACT

Oxide ionic conductivities of  $(CeO_2)_x(Sc_2O_3)_{(0.11-x)}(ZrO_2)_{0.89}$  (x=0.01-0.10) electrolytes were optimized for the application in intermediate-temperature solid oxide fuel cell (IT-SOFC). Powders with different contents of CeO<sub>2</sub> and Sc<sub>2</sub>O<sub>3</sub> were prepared via a co-precipitation method. The obtained powders and pellets were characterized by X-ray diffraction (XRD), scanning electron microscopy (SEM), energy dispersive spectroscopy (EDS) and impedance spectroscopy. Among all the compositions,  $(CeO_2)_{0.04}(Sc_2O_3)_{0.07}(ZrO_2)_{0.89}(4Ce7ScZr)$  gives the highest ionic conductivity of 0.065 S cm<sup>-1</sup> at 800 °C. The effects on densification and electrical properties of different sintering additives, such as SiO<sub>2</sub>, MgO, Co<sub>3</sub>O<sub>4</sub>, MoO<sub>3</sub> and Bi<sub>2</sub>O<sub>3</sub>, were studied and different conducting behavior with these additives were observed. The densification temperatures of CeO<sub>2</sub> and Sc<sub>2</sub>O<sub>3</sub> co-doped electrolytes can be reduced by around 280 °C with the addition of 1 mol% of Bi<sub>2</sub>O<sub>3</sub>, while the electrical properties of the electrolytes are not significantly affected by the introduction of Bi<sub>2</sub>O<sub>3</sub> aid.

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# 1. Introduction

Anode-supported solid oxide fuel cell with thin yttria-stabilized zirconia (YSZ, 8 mol%  $Y_2O_3$ ) as electrolyte is the mainstream for the operation in intermediate-temperature range (600–800 °C) [1–5]. However, the cell performance is too low when the cell runs below 700 °C. Developing new solid electrolytes with higher ionic conductivity for lower temperature application is necessary [6,7].

Among zirconia-based electrolytes, scandia-stabilized zirconia (ScSZ) is a very promising candidate because it shows appropriate thermal expansion, good mechanical properties and the highest oxide ionic conductivity due to the similar ionic radius of the Sc<sup>3+</sup> dopant to that of the Zr<sup>4+</sup> host  $R = r_{Sc^{3+}}/r_{Zr^{4+}} = 1.03$  [8,9]. Generally speaking, larger dopants, such as CeO<sub>2</sub> [10,11] and Y<sub>2</sub>O<sub>3</sub> [7,10–15], is helpful to stabilize the cubic/tetragonal phase structure of ScSZ electrolyte down to room temperature. It was reported that the sample with 10 mol% of Sc<sub>2</sub>O<sub>3</sub> and 1 mol% of CeO<sub>2</sub> (1Ce10ScZr) exhibits the best oxide ionic conductivity and good stability during extended annealing period [11], where the 1 mol% CeO<sub>2</sub> is used as phase stabilizer as usual. However, as we know there is no reported investigation carried out to optimize the best ratio of CeO<sub>2</sub>/Sc<sub>2</sub>O<sub>3</sub>.

The sintering activity of ScSZ electrolyte is quite poor due to the similar ionic radius of  $Sc^{3+}$  and  $Zr^{4+}$ . Achieving full density by conventional sintering methods requires high sintering temperatures (up to about 1600 °C). The high temperature sintering results in microstructures with grain sizes in the micron range, which subsequently induces poor mechanical stability. Higher densification temperature of ScSZ than that of YSZ is also an obstacle for its application in SOFCs. It is desirable to use lower temperature sintering which is more compatible to obtain appropriate anode microstructures.

In this paper, the ratios of CeO<sub>2</sub> to Sc<sub>2</sub>O<sub>3</sub> of  $(CeO_2)_x(Sc_2O_3)_{(0.11-x)}(ZrO_2)_{0.89}$  (x=0.01-0.10) were investigated in order to obtain the best conducting electrolyte for IT-SOFCs. The structure and conductivity of the powders and pellets were investigated in detail with XRD, SEM, EDS and impedance spectroscopy. In addition, SiO<sub>2</sub>, MgO, Co<sub>3</sub>O<sub>4</sub> [16], MoO<sub>3</sub> and Bi<sub>2</sub>O<sub>3</sub> [17] were adopted as sintering aids for the optimized electrolyte (CeO<sub>2</sub>)<sub>0.04</sub>(Sc<sub>2</sub>O<sub>3</sub>)<sub>0.07</sub>(ZrO<sub>2</sub>)<sub>0.89</sub> in order to improve the sintering properties.

#### 2. Experimental

#### 2.1. Powder synthesis

High purity Ce(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O, Zr(OH)<sub>4</sub>, Bi(OH)<sub>3</sub>, SiO<sub>2</sub>, Mg(OH)<sub>2</sub>, Co(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O, MoO<sub>3</sub> were used as starting materials as purchased from Sinopharm Chemical Reagent Co., Ltd. Sc<sub>2</sub>O<sub>3</sub> was purchased from Rare-Chem Hi-Tech Corporation of China.

The co-precipitation method was adopted to prepare powders as reported [7,11]. The stock solution was prepared by dissolving stoichiometric  $Zr(OH)_4$  and

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Table I	
Sintering conditions and re	lative densities.

Sample nomenclature	Composition	Sintering condition	Relative density (%)
10Ce1ScZr	$(CeO_2)_{0.10}(Sc_2O_3)_{0.01}(ZrO_2)_{0.89}$	1580°C(10h)	97.7
9Ce2ScZr	$(CeO_2)_{0.09}(Sc_2O_3)_{0.02}(ZrO_2)_{0.89}$	1580 °C (10 h)	97.0
8Ce3ScZr	$(CeO_2)_{0.08}(Sc_2O_3)_{0.03}(ZrO_2)_{0.89}$	1580 °C (10 h)	102.0
7Ce4ScZr	$(CeO_2)_{0.07}(Sc_2O_3)_{0.04}(ZrO_2)_{0.89}$	1580 °C (10 h)	95.3
6Ce5ScZr	$(CeO_2)_{0.06}(Sc_2O_3)_{0.05}(ZrO_2)_{0.89}$	1580°C(10h)	98.9
5Ce6ScZr	$(CeO_2)_{0.05}(Sc_2O_3)_{0.06}(ZrO_2)_{0.89}$	1580 °C (10 h)	97.8
4Ce7ScZr	$(CeO_2)_{0.04}(Sc_2O_3)_{0.07}(ZrO_2)_{0.89}$	1500 °C (10 h)	99.4
3Ce8ScZr	$(CeO_2)_{0.03}(Sc_2O_3)_{0.08}(ZrO_2)_{0.89}$	1580 °C (10 h)	100.4
2Ce9ScZr	$(CeO_2)_{0.02}(Sc_2O_3)_{0.09}(ZrO_2)_{0.89}$	1580 °C (10 h)	100.4
1Ce10ScZr	$(CeO_2)_{0.01}(Sc_2O_3)_{0.10}(ZrO_2)_{0.89}$	1580°C (10 h)	100.0

Sc<sub>2</sub>O<sub>3</sub> in hot nitric acid. The required quantity of Ce(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O was then added to the solution. Precipitation was carried out by adding ammonia to the solution under vigorously stirring. The pH value was controlled within 9–10 at the end with a pH detector. After pumping filtration, the precipitate was rinsed thoroughly with hot alcohol until most of the ammonia and water was eliminated during heating and finally dried in an oven at 110 °C for 24 h. In the case of the samples containing sintering additive, the additive was mixed with the stock solutions before co-precipitation. The powders obtained from the co-precipitation method were calcined, and then planetary ball milled with zirconia balls for 24 h. The obtained powders were uniaxially pressed into discs with a diameter of 8 mm and a thickness of 1–2 mm under 300 MPa. The pressed pellets were then sintered at a certain temperature from 1300 °C to 1580 °C, most for 10 h and some for 5 h.

#### 2.2. Powder characterization

Phase structures of powders were characterized using XRD technique and the data were collected using a Bruker D8 Advance (Germany) with Cu K $\alpha$  radiation at a step of 0.02° s<sup>-1</sup> in the range of 2 $\theta$  from 20° to 80°. The sintered pellets were observed by SEM (Hitachi, S-4800, Japan). The relative density of the sintered pellets was determined *via* Archimedes' method. The oxide ionic conductivity of the pellets was measured using a frequency response analyzer (FRA, Solartron 1260) over a frequency range of 0.1 Hz to 1 MHz at temperature range of 450–850°C in air with Pt electrodes. The ionic conductivity,  $\sigma$ , was calculated from the impedance data and the activation energy ( $E_a$ ) of the conductivity was determined by the Arrhenius law:

$$\sigma T = \sigma_{\rm o} \exp\left(\frac{-E_{\rm a}}{kT}\right)$$

where  $\sigma_0$  was the pre-exponential factor and k was the Boltzmann constant. Table 1 gives the nomenclature, sintering temperature and relative density of all samples.

#### 3. Results and discussions

Fig. 1 gives XRD patterns for the powders with different ratios of CeO<sub>2</sub> to Sc<sub>2</sub>O<sub>3</sub>. As reported previously [8], 1 mol% of CeO<sub>2</sub> additive is sufficient for the stabilization of cubic phase of scandia-stabilized



Fig. 1. XRD patterns of sintered  $(CeO_2)_x(Sc_2O_3)_{(0.11-x)}(ZrO_2)_{0.89}$  (x = 0.01–0.10).

zirconia at high temperatures. Increasing the content of  $CeO_2$  thereafter does not induce additional phase. This is important for practical application as electrolytes for SOFC.

Fig. 2 compares the resistance contributions from the bulk and grain boundaries of each sample obtained at 450 °C. The total resistances of all sintered specimens vary with the doping amount of CeO<sub>2</sub>. The grain boundary resistances are much smaller compare to the bulk resistances in all samples. The low but relatively constant values of the grain boundary resistances show that the grain boundaries are free of the segregation of resistant impurity [7].

Fig. 3 gives the ionic conductivities of all the specimens tested at 800 °C. Each point in this graph is calculated by averaging at least two measurements for the sample. 4Ce7ScZr shows the highest conductivity ( $0.065 \,\mathrm{S \, cm^{-1}}$  at  $800 \,^{\circ}\mathrm{C}$ ). The conductivity of traditional electrolyte YSZ was also tested and the values of 4Ce7ScZr are higher than that of YSZ over the whole investigation temperature range, as shown in Fig. 4. When  $Sc_2O_3$  is co-doped with  $Y_2O_3$  at a total amount of 11 mol%, 2Y9ScZr gives the maximum conductivity  $(0.0589 \,\mathrm{S}\,\mathrm{cm}^{-1}, 800 \,^{\circ}\mathrm{C})$  [15]. In this study, considering the high cost of Sc<sub>2</sub>O<sub>3</sub>, we achieve a higher ionic conductivity with less amount of Sc<sub>2</sub>O<sub>3</sub> for the future mass production. Consistent with Fig. 2, a strange drop in the conductivity is observed at 5Ce6ScZr and ionic conductivity increases with the increasing CeO<sub>2</sub> at low content but decreases with the increasing CeO<sub>2</sub> at high content. This observation is also found in  $(Y_2O_3)_x(Sc_2O_3)_{(0.11-x)}(ZrO_2)_{0.89}$  electrolyte material, with an inconsistency at the middle point 5.5Y5.5ScZr [15]. The reason is not fully understood.

Other than the conductivity, sintering property of scandiastabilized zirconia is an important issue. As shown in Table 1, the achievement of density as high as above 95% for all the specimens



**Fig. 2.** Total, bulk and grain boundary resistivities of the  $(CeO_2)(Sc_2O_3)_{(0,11-x)}(ZrO_2)_{0.89}$  (x=0.01–0.10) system as a function of the CeO<sub>2</sub> content, recorded at 450 °C.



**Fig. 3.** Ionic conductivity of the  $(CeO_2)_x(Sc_2O_3)_{(0.11-x)}(ZrO_2)_{0.89}$  (*x* = 0.01–0.10) system, recorded at 800 °C.



Fig. 4. Arhenius plots of YSZ and 4Ce7ScZr.

without sintering aids requires high temperatures over 1580 °C for 10 h. Lower sintering temperature results in lower density.

In order to lower the desification temperature, SiO<sub>2</sub>, MgO, Co<sub>3</sub>O<sub>4</sub> [16], MoO<sub>3</sub> and Bi<sub>2</sub>O<sub>3</sub> [17] are introduced into the sample 1Ce10ScZr as potential sintering additives. Table 2 summarizes the sintering conditions and sample densities. With the introduction of Co<sub>3</sub>O<sub>4</sub> and Bi<sub>2</sub>O<sub>3</sub>, the sample can reach full densification at a temperature as low as 1300 °C. The introduction of SiO<sub>2</sub>, MgO and

#### Table 2

Sintering properties for 1Ce10ScZr with different sintering additives.



**Fig. 5.** Conductivity-temperature plots of specimens with introduction of different sintering addictives. (a) One stage kind and (b) two stages kind.

 $MoO_3$  results in a slightly lower density even though the samples are also sintered at 1580 °C.

Fig. 5 gives the ionic conductivity behavior of the electrolytes with different sintering additive. These five sintering additives can be divided into two categories according to their performances: one stage and two stages. SiO<sub>2</sub>, MgO and MoO<sub>3</sub> belong to the one stage group because the conductivity–temperature plots of the specimen are all in a straight line. Meanwhile,  $Co_3O_4$  and  $Bi_2O_3$  are grouped to the two-stages group. The samples with SiO<sub>2</sub>, MgO and MoO<sub>3</sub> give higher  $E_a$  than the samples with  $Co_3O_4$  and  $Bi_2O_3$  and thus have lower conductivities. Therefore, SiO<sub>2</sub>, MgO and MoO<sub>3</sub> are not suitable sintering aids. As for  $Bi_2O_3$ , liquid  $Bi_2O_3$  appears at above 650 °C, which accelerates the conduction of oxygen vacancy, and the electrolyte show different conduct-

Sample nomenclature	Composition	Sintering condition	Relative density(%)
1Ce10ScZr-1300	1 mol% CeO <sub>2</sub> + 10 mol% Sc <sub>2</sub> O <sub>3</sub> + 89 mol% ZrO <sub>2</sub>	1300°C(10h)	83
1Ce10ScZr-1400	1 mol% CeO <sub>2</sub> + 10 mol% Sc <sub>2</sub> O <sub>3</sub> + 89 mol% ZrO <sub>2</sub>	1400 °C (10 h)	90
1Ce10ScZr-1500	1 mol% CeO <sub>2</sub> + 10 mol% Sc <sub>2</sub> O <sub>3</sub> + 89 mol% ZrO <sub>2</sub>	1500°C(10h)	96
1Ce10ScZr-1580	1 mol% CeO <sub>2</sub> + 10 mol% Sc <sub>2</sub> O <sub>3</sub> + 89 mol% ZrO <sub>2</sub>	1580 °C (10 h)	100
1Ce10ScZr-Si-1580	(1 mol% CeO <sub>2</sub> + 10 mol% Sc <sub>2</sub> O <sub>3</sub> + 89 mol% ZrO <sub>2</sub> ) + 0.5 mol% SiO <sub>2</sub>	1580 °C (10 h)	96
1Ce10ScZr-Mg-1580	(1 mol% CeO <sub>2</sub> + 10 mol% Sc <sub>2</sub> O <sub>3</sub> + 89 mol% ZrO <sub>2</sub> ) + 5 mol% MgO	1580 °C (10 h)	92
1Ce10ScZr-Mo-1580	(1 mol% CeO <sub>2</sub> + 10 mol% Sc <sub>2</sub> O <sub>3</sub> + 89 mol% ZrO <sub>2</sub> ) +5 mol% MoO <sub>3</sub>	1580°C (10h)	96
1Ce10ScZr-Co-1300	(1 mol% CeO <sub>2</sub> + 10 mol% Sc <sub>2</sub> O <sub>3</sub> + 89 mol% ZrO <sub>2</sub> ) + 2 mol% Co <sub>3</sub> O <sub>4</sub>	1300°C(10h)	100
1Ce10ScZr-0.5Bi	(1 mol% CeO <sub>2</sub> + 10 mol% Sc <sub>2</sub> O <sub>3</sub> + 89 mol% ZrO <sub>2</sub> ) + 0.5 mol% Bi <sub>2</sub> O <sub>3</sub>	1300 °C (5 h)	98
1Ce10ScZr-1Bi	(1 mol% CeO <sub>2</sub> + 10 mol% Sc <sub>2</sub> O <sub>3</sub> + 89 mol% ZrO <sub>2</sub> ) + 1 mol% Bi <sub>2</sub> O <sub>3</sub>	1300 °C (5 h)	101
1Ce10ScZr-3Bi	$(1 \text{ mol}\% \text{ CeO}_2 + 10 \text{ mol}\% \text{ Sc}_2\text{O}_3 + 89 \text{ mol}\% \text{ ZrO}_2) + 3 \text{ mol}\% \text{ Bi}_2\text{O}_3$	1300 °C (5 h)	100



Fig. 6. XRD patterns of 1Ce10ScZr-1Bi and 11Ce10ScZr-3Bi.

ing mechanisms compared with the one at lower temperature. For  $Co_3O_4$ , it is decomposed partially to CoO with O element released above 700 °C. An endothermatic peak can be detected by thermal analysis. The decomposition significantly accelerates the vacancy conduction. Therefore, two stages with different  $E_a$  appear in the conductivity–temperature curves of electrolytes with Bi<sub>2</sub>O<sub>3</sub> and Co<sub>3</sub>O<sub>4</sub>. The introduction of Bi<sub>2</sub>O<sub>3</sub> does not change the ionic conductivity of 1Ce10ScZr (0.040 S cm<sup>-1</sup>, 800 °C) obviously. However, the introduction of Co<sub>3</sub>O<sub>4</sub> lowers the ionic conductivity of the sample.

The effect of the  $Bi_2O_3$  amount on conductivity is also investigated. When 0.5 mol%  $Bi_2O_3$  is added, the diffusion of  $Bi_2O_3$  in the sample is not enough and inhomogeneous, which can be observed by eyes. As a result, a slightly lower density is observed. 1 mol%  $Bi_2O_3$  is necessary in order to ensure the homogenous distribution, which resulted in a fully dense sample. When 3 mol%  $Bi_2O_3$  is used, new peaks for face-centered cubic phase of  $Bi_2O_3$  can be detected by XRD, as shown in Fig. 6. As a result, the ionic conductivity at 800 °C of 1Ce10ScZr–3Bi is lowered to 0.036 S cm<sup>-1</sup>, showing a 10% drop from 0.040 S cm<sup>-1</sup> of 1Ce10ScZr–1Bi. Therefore, 1 mol%  $Bi_2O_3$  addition is chosen as an optimal amount for CeScZr electrolyte.

In our study, 1 mol%  $Bi_2O_3$  is also used in the best composition 4Ce7ScZr, as shown in Fig. 3. The ionic conductivity of 4Ce7ScZr–1Bi is 0.067 S cm<sup>-1</sup> at 800 °C, which is close to 0.065 S cm<sup>-1</sup> for 4Ce7ScZr. However, 4Ce7ScZr–1Bi can be fully densified at 1300 °C other than 1580 °C.

Fig. 7 shows the SEM micrographs of the cross-section and surface of 1Ce10ScZr–1Bi. The grain boundary on the surface is unclear and the grain size is as large as  $6 \,\mu$ m even sintered at 1300 °C. This is due to the liquid sintering mechanism. In grain boundaries, some small particles can be found as marked in Fig. 7b. Table 3 lists the data of elemental analysis by EDS of these small particles. Higher Bi<sub>2</sub>O<sub>3</sub> content can be observed in the marked area than other, suggesting Bi<sub>2</sub>O<sub>3</sub> agglomeration at grain boundary. Densi-

#### Table 3

Elemental analyses by EDS of the selected area of 1Ce10ScZr-1Bi sintered at 1300  $^\circ\text{C}$  for 5 h.

Element	Wt%	At%
СК	9.61	29.55
OK	15.80	36.45
ZrL	56.18	22.74
BiM	1.79	0.32
ScK	11.77	9.66
CeL	4.85	1.28



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Fig. 7. SEM and of 1Ce10ScZr-1Bi at 1300 °C for 5 h: (a) surface and (b) cross-section.

fication mechanism is mainly due to the characteristics change at grain boundary instead of lattice structure [18]. As confirmed by EDS map in Fig. 8, the concentration of Zr element decrease obviously at the contact part of several grains, thereby leading to a relative increase of Bi, Sc and Ce concentration.



Fig. 8. EDS maps of a selected area of 1Ce10ScZr-1Bi at 1300 °C for 5 h.

# 4. Conclusions

In this work,  $(CeO_2)_x(Sc_2O_3)_{(0.11-x)}(ZrO_2)_{0.89}$  (x=0.01-0.10) with various ratios of  $CeO_2$  to  $Sc_2O_3$  were synthesized and characterized. 4Ce7ScZr shows the maximum conductivity of 0.065 S cm<sup>-1</sup> at 800 °C, which can be a good candidate for IT-SOFCs. Bi<sub>2</sub>O<sub>3</sub> is proven to be a good sintering aid to synthesize scandia-stabilized zirconia. 1 mol% of Bi<sub>2</sub>O<sub>3</sub> addition to the electrolyte can reduce the densification temperature greatly and does not affect the ionic conductivity significantly. 4Ce7ScZr with 1 mol% addition of Bi<sub>2</sub>O<sub>3</sub> is promising as the electrolyte candidate for IT-SOFC.

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